Determination of Martian Surface Reflectivity> From 0.4 to 1.1 Micron Using a Vidicon Spectrometer

by

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Certified by:____

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Accepted by:_

Chairman, Departmental Committee on Graduate Students

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ABSTRACT

A new astronomical instrument, the vidicon spectrometer, is being developed at the M.I.T. Planetary Astronomy Laboratory. Based on the silicon diode vidicon system currently in use there. a low dispersion prism is added between the vidicon image tube and the telescope, allowing digital vidicon photographs to be taken of These spectra are stored on magnetic tape and computer spectra. processed to create intensity vs. havelength curves for stars and The high spatial resolution of the vidicon image tube, planets. combined with a higher spectral resolution than photometer filters currently in use at M.I.T. give this instrument potential in the study of planetary surface composition from spectral reflectivity. Procedures for reducing the vidicon images to spectra have been tested on a set of spectra of two stars and the planet Mars. 1 t is concluded that the vidicon response is not linear enough with variations in exposure time at lou levels of incoming light for consistent star spectra, although it works well with Mars due to the planet's larger intensity where the vidicon tube has its The spectrometer slit is so narrow (one second poorest response. of arc for this data) that uavelength-dependent variations in refraction of light from a point source by the atmosphere cause star spectra of variable quality. Because of the low quality of the star spectra, direct spectral reflectivity measurements (which are obtained using Mars to star ratios) proved to be impossible. Although further tests of the spectral and intensity response of the silicon diode vidicon should be carried out in the laboratory before good results can be guaranteed, the present Mars spectra may probably be used in conjunction with photometer-derived reflectivity data to expand coverage of the surface of Mars.

Thesis Advisor: Thomas B. McCord

Title: Associate Professor of Planetary Physics

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I. Introduction

Although Mariner 9 has returned a vast quantity of information about the planet Mars, little was learned about surface composition. From such experiments as the infrared spectrometer, particle size and silica composition were estimated, but these determinations had error bars so great as to be nearly useless in reaching conclusions about the composition of the surface materials of Mars. Until the Viking Lander in 1976, there is no way to physically look at a Martian rock with instruments.

Probably the most useful technique for remotely sensing surface composition is reflectance spectroscopy. Dollfus (1961), studying the polarization of light reflected by Mars, concluded that limonite, a hydrated iron oxide, was probably a major Hovis (1965) observed absorption bands in the nearconstituent. infrared reflectivity of limonite and suggested that they would be a diagnostic test for limonite on Mars. Sagan et al (1965) compared absorption bands they observed in laboratory specimens of Limonite to Dollfus' Martian albedo curves and concluded that a surface with at least some limonite was not inconsistent with the Adams (1968) observed absorption bands between 0.5 and 2.5 data. microns in many iron-bearing minerals, the positions of which varied significantly from mineral to mineral. These bands are caused by electron transitions in iron ions and by vibrational bands in hydroxyl ions and water molecules. Adams suggests that the absorption feature observed in Tull's (1966) geometric albedo curve is not inconsistent with a hydrated basalt composition. The feature observed at one micron in their spectra is not due to iron in iron oxides, but to iron ions in silicates. Adams and McCord (1969), using geometric albedoes obtained during the 1967 opposition discovered that curves for the bright areas had different shapes than those from the dark areas of the Martian surface. They concluded that the surface was composed of a combination of oxidized basalt and hydrated iron oxides. The bright and dark areas were modelled as being composed of of the same material in different degrees of oxidation.

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McCord and Westphal (1971, see also McCord, Elias, and Westphal, 1971) observed Mars during the 1969 opposition and noted that the iron ion absorptions were in different places, indicating compositional differences. Seven areas were observed, four dark and three bright, each being about five Martian longitudinal degrees in diameter. From this data, much compositional analysis has been done (see Figure 1 for examples of mineral reflectivities Mars); however, small sample, compared to from such а deneralizations about the rest of the surface cannot be made. Despite over twenty additional spots obtained during the 1973 opposition, such interesting features as the Coprates canyon and the Hellas basin remain uncovered; what is needed is whole disk coverage at high spectral and spatial resolution. A new technique, vidicon spectroscopy, has been developed to obtain the



Figure 1.

Comparison of Mars dark area reflectivity to reflectivity of sheet silicates. Note resemblance to the clay minerals, kaolinite and montmorillonite.

(Courtesy Dr. Robert Huguenin)

desired high resolution full-disk coverage. This thesis describes that technique.

II. The Vidicon Spectrometer

The silicon diode array vidicon was originally developed for television and picturephone use, but because of its large dynamic range, high quantum efficiency, and linear response, it is being used by a growing number of astronomers as a digital replacement for photographic plates. The only advantage a photographic plate has over a vidicon is spatial resolution; however, that is not a limiting factor as atmospheric conditions are the resolutionlimiting factor in astronomy. McCord and Westphal (1972), Kunin (1972), and McCord and Bosel (1973) have reported on the development of a vidicon system for single-frame astronomical photography at the Planetary Astronomy Laboratory of the Massachusetts Institute of Technology (MITPAL). This system is based on an RCA silicon vidicon tube with a peak quantum efficiency of 85% at 0.5 microns, sloping off to about 6% at 1.1 microns (see Figure 2). Using filters this system has been developed as a two-dimensional imaging photometer, using filter. sets similar to those used with photometers for spectral reflectivity work at MIT. As reported by McCord and Bosel, a vidicon spectrometer which would give the spatial resolution of the vidicon combined with a greater spectral resolution than such a vidicon photometer is under development.

The vidicon spectrometer is basically an optical system which is attached to the front end of the vidicon system on the telescope. Schematically it consists of a low-dispersion prism



through which light from a slit situated at the focus of the telescope is passed. The dispersed image of the slit is then refocused onto the surface of the vidicon diode array. In practice this is done through a system of mirrors (see Figure 3 for details) to avoid the infrared absorption of lenses.

The vidicon tube consists of a 1024 by 1024 array of reverse biased diodes. A photon impinging on the vidicon target results in a decrease in charge in the diode it reaches. The image is read out by scanning the diode array with an electron beam which recharges the diodes as it hits them, producing a current proportional to the amount of charge lost. By knowing where the beam is at any given time, the intensity at each location in the diode array can be known. These intensity elements are then passed on to be recorded and displayed (for further details on the electronics of a silicon vidicon see Crowell and Labuda (1963)). The vidicon is read out as 250 rous of 256 image elements, each of which corresponds physically to four diodes. In such a lower resolution scan. less accurate positioning is required of the No data is lost, and the vidicon's resolution is electron beam. still better than the atmosphere allows. The intensity image is amplified, recorded on magnetic tape, and displayed on a slow scan This image is then available for further computer TV monitor. processing. The spectrometer system is diagrammed in Figure 4.

A portion of a vidicon spectrometer image is presented in Figure 5. The elements along the column correspond to spatial



Figure 3. Optics of the MITPAL vidicon spectrometer. The telescope is to the right.



Figure 4. The MITPAL vidicon system with the spectrometer attached.

elements along the slit. Wavelength is along the abscissa. The magnitude of each element is proportional to the current from the vidicon diode array at the time a corresponding diode was read by the scanning electron beam. The image is now ready to be turned into a spectrum.

PAP SL	1	171	1.00	1.7.4	1.0	1.8-1	142	1.0	1.44	145	186	1.97	194.	189	190	191	192	193	194	195	196	197	198	149	20-0
1-	1.1	553		567	559	553	564	561	560	559	547	550	559	558	556	556	554	565	556	552	558	557	546	549	555
7-	745	255	24.1	165	243	253	747	244	741	742	240	243	240	240	238	233	246	239	246	245	252	238	246	243	240
3-	149	194	1.7.1	190	197	192	193	192	144	190	189	188	179	183	101	198	186	195	186	196	195	187	198	189	191
4-	165	161	1.1	173	171	167	164	171	141	174	102	175	166	156	167	165	163	161	176	164	172	172	156	165	154
5-	159	161	157	157	155	157	167	164	11.4	152	158	170	166	159	153	157	150	157	164	154	170	169	164	112	115
-3	152	158	156	152	157	135	146	157	160	155	160	163	159	163	161	165	163	166	157	162	157	175	170	156	185
7-	146	137	157	147	154	155	152	158	153	144	149	158	151	157	-141	144	159	157	101	154	165	103	111	109	175
- 5	157	149	156	150	159	153	157	163	158	155	162	145	157	155	157	1 9 1	100	170	101	120	175	100	194	102	170
9-	151	162	159	154	161_	163	151	-152	174	167	103	154	173	160	172	179	176	190	197	181	181	199	189	184	194
10-0	165	162	119	165	172	183	170	107	100	210	200	212	202	210	202	219	206	209	209	203	205	197	199	208	200
11-	718	197	CGE.	-115	269	1.19	202	264	117	125	122	117	111	295	298	300	284	273	258	245	247	240	217	226	228
12-	341	354	3.13	361	4.25	630	627	620	607	573	570	557	552	535	506	476	452	422	380	347	325	317	361	299	267
1.3-	2.1	0.1.	613	010	622	6.6.4	677	6.35	659	044	656	653	645	641	614	591	572	523	473	431	409	391	375	347	312
15-	5.57	1771	1227	1347	1245	124.9	1276	1245	1190	1144	1127	1131	1099	1047	1012	972	919	848	735	645	.609	582	545	47.2	417
	1040	2110	2140	2128	2147	2179	2191	2172	2099	2048	2047	2040	2016	1950	1878	1795	1711	1562	1311	1165	1102	1035	935	805	653
17-	2611	2453	2699	2500	2520	2545	2567	2549	1484	2439	2425	2439	2417	2360	2304	2219	2123	1967	1687	1541	1506	1458	1295	1120	959
19-	16.1	2515	2532	2.31	2550	21.114	2625	2617	2540	2487	2451	2484	2459	2416	2323	2285	2185	2042	1788	1648	1625	1508	1449	1291	1111
17-	2425	2471	24.73	2574	2503	2544	2567	2547	2489	2433	2444	2449	2417	2357	22.97	2228	2138	2019	1768	1647	1607	1551	1457	1309	1136
20-	2399	7419	24.55	241.0	2411	2512	2544	2534	2460	2401	2400	2397	2377	2304	2271	2207	2112	1968	1750	1615	1583	1542	1427	1279	1138
11-	2215	2354	2314	2384	1985	2437	2459	2459	2384	2339	2360	2356	2324	2265	5501	2127	2047	1932	1706	1567	1558	1497	1388	1242	1094
22-	11.3	2233	1:14	1132	2241	2230.	2312	5 10 3	2225	2189	2194	5500	2185	2129	2075	5001	1927	1811	1610	1489	1455	1420	1311	1131	1045
13-	2174	2721	11:34	201.5	2295	232%	2331	2374	2213	2225	2704	2222	2208	8197	2088	2073	1937	1824	1011	14/1	14.14	1601	1211_	1234	1070
14-	2311	1:11	21.15	1.37	2441	2471	2488	2496	2432	2368	2368	2357	7343	2304	22.30	2114	20.11	1965	1007	1743	1710	1671	1532	14.4	1195
25-	1.40	2- 1-	1.15	3.27	71.43	2764	2747	2/33	2656	2592	2581	2611	2542	2001	1626	2401	2212	2113	1904	1152	1124	15/8	1561	1401	1235
16-	144 .	14.11	2446	1.01	2014	2010	2011	2000	2021	2768	2744	2717	2723	2675	26.01	2529	2457	2313	2044	1900	1869	1805	1691	1527	1351
21-	1115	2005	1 20	1. 20	30.51	3114	3151	3159	30/3	3017	3021	3045	3041	2960	2869	2816	2708	2570	2265	2083	2073	2028	1958	1653	1480
20-	2047	1 10 1	1.11	1165	3073	3127	3160	3191	3113	3040	3056	3075	1057	2992	2920	2841	2776	2609	2303	2121	2109	2062	1919 -	1744	1535
	11	11 1.	110	1141	3152	3208	3268	3249	3184	3112	3121	3139	3120	3056	2492	2929	2800	2686	2345	2156	2147	2108	1965	1743	1568
31-	2889	2748	39.50	\$222	3052	3120	3165	3192	3124	3045	3052	3064	3058	2971	2912	2835	2752	2631	2302	2143	2101	2047	1000	1724	1531
31-	18:5	2012	2991	2136	2911	3006	\$6,43	3066	3641	2955	2941	\$969	2944	2881	2805	5109	2011	2520	2232	2053	2017	1951	1424	1600	1470
13-	217)	274.5	21:10	24.17	2860	2915	2111.	2076	2935	2861	2858	2865	2848	2776	2689	2617	2535	2471	2145	1971	1936	1407	1703	1005	1427
34-	1517	2354	2421	2451	2488	2552	2589	2587	2556	2499	2510	2544	7524	2467	2418	2334	2245	2119	1866	1732	1/12	1631	1505	1424	1268
15-	1922	2030	2011	2:12	1968	508T	2128	2113	2083	2035	2043	2057	2034	1996	1936	1887	1333-	1740	1555	1444	1412	1189.	1407	11.1	1123
- 36-	2321	2341	1458	2451	241,0	2411	2539	2548	2496	2432	24.35	2444	2432	2384	2319	2249	2164	2055	1000	17.3	1710	1007	1571	1421	1263
31-	2.41	5:03	2244	6. 16	2519	25.52	2641	2020	2071	2417	2461	2465	2627	2571	2536	2680	2606	2201	2015	1843	1827	1777	1652	1476	1293
44-	2525	1580	2017	25.58	2001	25110	2603	2103	2120	2517	2501	2544	2528	2468	26.28	2356	2403	2179	1932	1784	1774	1741	1617	1466	1279
311-	2545	2493	24.91	2 41	21.47	21.35	2741	271.8	2721	2643	2641	2561	2652	2605	2534	2456	2411	2305	2032	IPAD	1855	1803	1017	1517	1324
61-	1.17	2193	2423	2461	2484	25,44	2577	2577	2540	2464	2481	2535	2528	2465	2403	2327	2276	2195	1924	1757_	1765	1724	1613	1456	1212
47-	1416	2692	1513	2536	2556	2617	2647	2676	2621	2569	2565	2607	2606	2544	2471	2412	2346	1240	1910	1819	1793	1768	1654	1483	1306
43-	143%	2401	1435	2447	24:12	2551	2549	2504	2567	2505	2524.	2560	2547	2502	2432	2373.	2292	220d.	1925	1787	1761_	17.36	1609	1451	1295
44-	11.94	174%	2130	2 11 5	2332	2391	2433	2456	2 195	2343	2357	2393	2381	2329	2289	2233	2160	2055	1819	1673	1651	1614	1505	1368	1228
45-	1.41	/11/	21.03	21.50	21:15	2241	2282	2228	21.63	2217	2224	2240	5532	2172	2113	2011	2012	1921	1661	1544	1526	1494	1389	12:4	1115
	1:11	1441	16,55	1469	1859	1.010	1748	1955	1920	1.887	1897	1919	1209	1876	1811	1769	1718	1642	1454	1335	1 328	1276	11.11	1087	969
-47-	1135	1112	1111	THT	1321	1:52	1870	1975	1849	1191	1791	1923	1805.	1122	1696	1658	TOC3	1517	1328	1220	1204	- Que	Rut	-107	129
4.4	1 11.4	1349	12/3	116.8	1374	1415	1435	1438	1406	1379	1 190	1409	020	011	1340	1.101	871	830	754	121	715	711	673	630	572
	e14	092	. 611	214	921	. 935		714	709	- 12L	612	690	696	6.8.0	671	660	616	608	565	540	522	519	492	406	423
50-	1.5%	517		1.00	614	609	517	620	520	511	511	519	504	500	408	494	474	451	417	397	393	_ 395	3/8	342	326
21-		1.0				3/4	3112	186	383	372	376	387	378	372	375	364	361	351	327	307	314	305	289	272	207
S. 6.1-	21.7	21.1	211	.216	274	245	227	293	281	217	283	291	283	281	254	279	273	273	251	255	244	_245	240	226	222
	21	211	214	124	224	2 10	223	225	221	218	224	230	228	222	217	214	214	213	212	201	206	503	202	203	190
55-	185	191	199	201	192	192	190.	198	_196	199	_194	192.	_ 191	195	193	_193	186.	_ 185.	_186_	_177.	_177_	_182	182	184	160
>1	184	177	120	141	191	17 5	177	185	180	181	182	175	177	172	187	179	178	184	179	173	176	168	173	183	176

Figure 5. A portion of one vidicon spectrometer image of Mars. It runs from about 0.6 μ in the leftmost column to 0.8 μ in the rightmost.

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III. Image Processing

The first processing that must be done to the image is to convert the column coordinate into wavelength. This is done through the use of a calibration function:

$$S = -S_0 + \frac{C}{(\lambda - \lambda_0)} \qquad \qquad \lambda = \lambda_0 + \frac{C}{(S + S_0)}$$

 S_0, λ_0 , and C being three constants determined from three column number-wavelength correspondences as follows:

$$C = \frac{(\lambda_1 - \lambda_2) (S_1 + S_0) (S_2 + S_0)}{(S_2 - S_1)}$$
$$S_0 = -S_1 + \frac{(\lambda_2 - \lambda_3) (S_2 - S_1) (S_3 - S_1)}{(\lambda_1 - \lambda_2) (S_3 - S_2) - (\lambda_2 - \lambda_3) (S_2 - S_1)}$$

$$\lambda_0 = \lambda_1 - \frac{C}{(S_1 + S_0)}$$

These correspondences are obtained by observing the spectrometer image of a calibration lamp with known sharp emission lines (as shown in Figure 6). From this calibration, which is redone periodically as data is taken, the wavelength-column relationship is known (see Figure 7 for an example). The resolution also varies as a function of wavelength, as would be expected (see Figure 8 for a sample dispersion function plotted from the first derivative of the calibration function).

Now enough is known to process a spectral image. A program



VIDC	52 F	.125								
51=	35.	0 L1= 0.3	37 SZ=	57.5 L2	= 0.35	7 53= 199	.5 L3=	0.809		
LC=	0.1	541 C=-4	1.7388	S0=-263	.2354					
	1	0.3133	51 .	C.3508	101	0.4114	151	0.5260	201	0.8248
	2	0.3139	52	0.3517	102	0.4130	152	0.5294	202	0.8357
	3	0.3145	53	0.3527	103	0.4146	153	0.5328	203	C.8471
	4	C. 31 -1	54	0.3536	104	0.4162	154	0.5362	204	0.8588
	5	0.3158	55	0.3546	105	0.4179	155	0.5398	205	0.8708
	6	0.3104 .	55	0.3555	106	0.4196	156	0.5433	206	C.8834
	7	0.3170	57	C.3565	107	. 0.4213	157	0.5470	207	0.8963
	8	0.3177	58	0.3575	108	0.4230	158	0.5507	208	0.9098
	9	C. 31.33	59	0.3585	109.	0.4247	159	0.5546	209	0.9237
	10	0.3169	60	C.3075	110	0.4265	160	0.5584	210	C.9382
	11	0.3196	. 61 .	0,3605	111	0.4283	161	0.5624	211	0.9532
	12	0.3203	62	0.3615	112	0.4301	162	0.5654	212	0.9688
	13	0.3209	63	0.3626	113	0.4319	163	0.5705	213	0.9850
	14	C. 3216	64	0.3636	114	0.4338	164	0.5747	214	1.0019
	15	0.3223	65	0.3047	115	0.4357	165	0.5790	215	1.0194
	10	0.3229	66	0.3657	116	.0.4376	166	0.5834	216	1.0378
	17	0. 32 36	67	1. 3668	117	0.4395	167	0.5878	217	1.0569
1. Las 7. 1	18	. 0.3243	68	0.3079	118	0.4415	168	0.5924	218	1.0768
	19	C. 3250	69	0.3690	119	0.4435	169	0.5970	219	1.0977
	20	U.3257	70	0.3701	120	0.4455	170	0.6018	220	1.1195
	11	0.3264	71	0.3712	121	0.4476	171	0.6066	221	1.1424
-	22	0.3271	72	0.3124	122	0.4497	172	0.6116	222	1.1663
	23	C. 3279	73	0.3735	123	0.4518	173	0.6167	223	1.1915
Free State	24	0.3286	14	0.3747	124	0.4537	174	0.6219	224	1.2179
1. 1. 1	25	0.3293	75	0.3759	125	0.4561	175	0.6272	225	1.2458
2.1	26	0.3301	76	0.3770	126	0.4583	176	0.6326	226	1.2751
1.1.1.	27	0.3308	77	0.3782	127	0.4605	177	0.6381	227	1.3060
1	28	0.3316	.78	0.3795	128	0.4628	178	0.6438	228	1.3387
25	29	. 0.3323	79	0.3807	129	0.4651	179	0.6496	229	1.3733
28 10 . H	30	0.3331	80	0.3019	130	0.4674	180	0.6556	230	1.4100
19.5	31	0.3339	81	0.3832	131	0.4698	181 .	0.6617	231	1.4489
	32	0.3346	82	0.3844	132	C.4727	182	0.6679	232	1.4904
	33	C. 3354	. 83	0.3857	133	0.4746	183	0.6743	233	1.5346
	34	0.3362	84	0.3870	134	0.4/71	184	0.6809	234	1.5818
	35	0.3370	85	0.3883	135	0.4796	185	0.6876	235	1.6324
16.1	36	0.3378	86	0.3396	1.36	0.4322	186	0.6945	236	1.6866
	37	0.3336	87	0.3910	137	0.4848		0.7016	237	1.7451
	38	0.3374	88	0.3723	138	0.4874	188	0.7089	238	1.8081
-	39	C. 3403	83	0.3931	139	0.4901	189	0.7164	239	1.8764
	40	0.3411	90	0.3451	140	0.4928	190	0.7241	240	1.9505
	41	0.3419	91	0.3965	141	0.4956	191	0.7319	241	2.0313
	42	0.3428	92	0.3979	142	0.4984	192	0.7401	242	2.1197
÷	43	0.3436	93	0.3993	143	0.5013	193	0.7484	243	2.7168
	44	0.3445	94	0.4008	144	0.5042	194	0.7570	244	2.3240
	45	.0.3454	.95	0.4022	145	0.5071	195	0.7658	245	2.4430
	40	0.3463	95	0.4037	146	0.5101	196	0.7749	246	2.5758
· ····································	47	0.3471	. 91	0.4052	147	0.5132	197	0.7843	247	2.7250
1200	48	0.3480	98	0.4157	148	0.5163	198	0.7939	248	2.8937
Sec. and	49	0.3490	99	0.4083	149	0.5195	199	0.8039	249	3.0862
a second	.50	0.3499	100	0.4098	150	0.5227	200	0.9142	250	3.3077

re 7. Wavelength as a function of vidicon column for a typical calibration function. The three column (Sn)-wavelength (Ln) pairs used to determine the function are given at the top. Column number is at the left, wavelength at right.

Figure 7.



has been written which runs as a subroutine under the Planetary Astronomy Laboratory's image processing system (DIPSYS) which has been set up to provide a metastructure under which vidicon images may be easily processed. A simplified diagram of this program. appears in Figure 9. The spectral image is read off the run tape by DIPSYS and stored on a disk where it is available to the spectral processing routine, which has three basic tasks. The first and easiest is to punch out the intensities along one rou of the image onto computer cards for input into a plotting routine (this was how Figure 6 was produced). Second, it can subtract the average background from the image, column by column, where the rows over which the background is to be averaged are read from the input instruction cards. Last, and most important, the program can produce a new image in which all of the elements have the same spectral resolution. For spectral reflectivity work, where the range of interest is 0.4 to 1.2 microns, a resolution of 250 angstroms, the best resolution at 1.2 microns, was chosen. Figures 10 and 11 show the effects of this processing on an image of the standard star Xi 2 Ceti. Portions of these images are then integrated spatially along the slit. Due to atmospheric and telescope optical effects, a star image is not a point; it is smeared out spatialy into to a Gaussian distribution of intensity which is at its maximum where the point source would be. To use the full energy output of the star at a given wavlength, the image must be integrated across all rows where the image intensity is

DIGITAL IMAGE DATA PROCESSING LINEPRINTER IMAGE TAPE SYSTEM DISK STORAGE SPECTROMETER IMAGE **VIDICON IMAGES** PROCESSING PROGRAM PUNCH ONE ROW SPECTRALLY RESOLVED OF IMAGE IMAGES SUBTRACT BACKGROUND SAVE IMAGE LINEPRINTER PLOT OF SPECTRUM Figure 9. CREATE SPECTRALLY Structure and inter-**RESOLVED IMAGE AND** PUNCHED CARDS action of the vidicon SAVE IT spectrometer image processing programs. SUM ACROSS PORTION OF IMAGE AND SAVE MAGNETIC TAPE PLOTTING AND RATIO PROGRAMS CALCOMP PLOTS

:2.1	151	152	153	154	155	155	. 157	158	159.	160	101	102	163	164	155	165	167	16	151	113	171	112	173	1.74	17:
1-	440	437	4 \$6.	437	441	442	443	436	446	150	450	445	454	44/	44 1	449	140	421		144		4-1	++1		44/
2-	204	204	1 12	213	1 19	175	147	141	146	145	164	145	160	154	162	166	161	1.00	144	140	157	1.04	1	112	1.23
	135	150	150	147	169	1.7	1 19	149	151	152	141	144	145	151	145	145	14.3	155	151	14.5	-145	143	145	1	1
-	144	165	145	155	147	157	145	144	141	143	144	148	144	140	141	147	145	140	14:	145	142	1-5	1-2	1.1	144
	145	-145	-141	142	-157	145	144	133	134	141	Rel	135	141	131	145	144	144	155	141	1+4	1+1	134	1+1	115	142
7-	137	152	145	139	144	145	147	140	137	157	146	144	143	145	146	141	142	134	138	147	147	139	144	139	133
8-	142	134	126	133	121	127	125	136	139	137	131	123	131	135	136	121	141	131	135	123	127	143	135	131	1.1
9-	135	141	1 51	135	134	131	132	129	137	141	143	132	139	135	141	137	131	133	139	144	141	135.	1:7	151	131
10-	121	147	143	127	133	135	129	132	137	137	131	145	135	126	140	133	132	1 15	125	137	133	130	143	142	124
11-	132	126	121	177	127	130	127	134	130	136	141	135	127	123	127	130	151	135	175	1 42	143	1	1.55	121	12.
12-	133	132	127	137	141	145	135	132	143	136	135	129	135	130	121	136	125	121	136	135	122	124	132	137	130
13-	135	134	121	1 31	134	132	142	137	141	190	144	141	122	137	174	126	1 20	126	125	141	111	124	1	125	125
14-	132	125	1 2 1	130	133	145	111	142	127	127	146	134	141	129	141	131	130	144	1/3	131	1 1 3 3	1.0	1-2	1.1	137
16-	127	136	1 13	143	135	128	131	130	127	1 19	134	-111	134	131	134	131	142	150	139	141	121	117	1.0	131	14 .
17-	126	125	127	127	134	127	137	132	129	135	124	123	125	13/	136	123	125	127	127	120	113	120	1.3	1 1 -	13.
15-	127	135	130	123	127	133	127	138	130	130	137	136	136	127	140	132	128	1.53	127	134	1 14	124	126	131	1.'5
17-	1 39	140	132	135	1 32	125	135	1 15	131	137	139	125	130	139	137	132	143	12?	137	137	132	130	1 >4	1.55	151
20-	133	137	139	139	127	123	122	136	134	137	137	130	175	151	135	131	130	135	127	155	143	11.3	123	177	127
-15	137	140	135	131	121	133	137	130	135	141	130	137	125	136	1.15	127	136	135	137	141	145	141	1 19	1 11	131
22-	139	132	134	138	131	140	135	139	129	138	146	127	134	132	129	1/9	140	135	111	1.52	1+1	1 35	134	1 1 1	131
23-	134	135	121	131	141	137	124	-131	-133	136	142	175	126	-111	1120	111	1 2 3		113			-1/-	1.10	1 . 1	1 16
24-	131	129	134	143	131	171	1 34	1 30	120	120	117	111	111	144	126	1.74	114	1 3 5	1.2.1	1.4		111	1.1.4		194
- 23-	136	141	133	126	136	136	135	1 13	112	145	1 41	-112	122	145	146	124	127	120	125	122		1.7	1.25	1	179
27-	144	131	143	136	126	123	132	139	120	143	143	125	129	138	127	132	145	132	131	127	1	127	1 + 1	137	125
28-	144	143	130	1 30	143	139	134	142	131	133	143	133	126	136	127	136	138	121	1.56	1 +1	1	1 +1	140	1 15	133
29-	152	151	1 313	148	144	147	1 32	144	138	135	151	144	135	141	141	127	131	13;	13%	144	1 1 1	125	1	142.	13
30-	215	221	207	217	220	206	203	224	204	214	-215	- 207	207	264	266	. 199	. 500	1.1 4	1.40	1 1 1	1-2	11.57	1 .:	111	155
31-	705	707	1.1	112	115	701	677	097	995	691	696	680	656	654	639	626	619	614	602	579	233	12.1	5-7	120	543
32-	1926	1 324	1919	1741	1373	1935	1735	1938	1917	1923	1936	1904	1844	1362	1672	1312	1612	1731	1 74 9	1/22	1717	41.1	17-1	1012	1635
11-	1945	19431	140	1.57	1475	1276	1971	1415	1272	1944	1467	1310	1705	1700	177	1120	1100	1.001	1-11	1.10	1	1	1	4329	1677
15-	71.4	768	118	791	1.4	133	737	A 14	797	805	819	811	812	413	615	411	127	1091	1041	1 11		FAS	-1-	310	701
	41 3	411	416	470	4/5	4 3.)	4 36	411	444	443	450	442	44.0	455	450	401	40.5	401	45%		473	403	434	482	469
37-	241	242	244	159	21.4	255	248	255	250	252	208	206	253	260	269	257	20.3	271	259	259	271	2.7	250	263	270
38-	178	185	1/1	183	179	163	177	178	172	179	178	180	175	186	179	1/3	1/7	172	105	173	111	115	175	171	1:0
39-	147	154	143	143	1 51	135	135	141	135	142	141	145	177	136	139	133	136	134	131	131	140	131	1 .1	14 .	1 44
40-	143	131	135	137	137	1 34	135	127	153	141)	135	132	135	1 37	135	124	1 35	1 31	121	131	1.1	157	1 -	121	1.13
41-	136	135	121	129	127	121	120	125	127	135	134	127	127	144	133	127	134	125	127	1+1	<u>ii</u>	1.57	1.1	14'	133
42-	125	134	121	12:	1.15	1.32	1/1	131	132	121	131	125	122	120	111	130	121	130	125	133.	1/2	123	1.1	124	129
- 43-	131	134	125	121	131	125	136	120	131	131	1 47	1 12	126	141	127	127	120	131	121	1.41	135	122	1	1 3 3	110
45-	132	131	127	131	129	134	128	143	. 120	120	1 12	1 12	127	1 15	134	116	127	127	126	124	1 13	12.	120.	124	13.
46-	135	131	134	132	135	128	131	136	129	136	131	123	122	132	127	125	134	132	140	132	14.	1 13	1 45	1 15	135
47-	129	144	129	137	131	121	1 10	1.17	131	125	129	133	125	131	131	1 31	127	1 54	125	137	144	1 1 3	130	13.	14 %
48-	134	132	125	124	137	121	131	131	127	133	145	122	132	136	135	174	138	1 5 7	130	1 31	1 44	133	1.5	1.55	14.
. 49-	134	132	147	1 15	131	134	1 12	1 37	1 5 3	137	1 30	- 1 .1	126	141	132	117	131	125	123	133	149	1 37	1.7	104	137
>0-	133	137	143	131	1 :5	127	174	136	137	121	124	134	126	1 36	137	150	1 34	133	145	130	115	1.44	1	149	114
- 21-	_148	141	133	- 127	. 137	125	_121	_140	155	139	_136	- 127	1 30	1 34	129	124	153	-12)	129	_ 134	127	133	1 *	144	137
-20	121	125	127	135	129	135	132	137	132	125	127	137	127	1.57	134	135	121	135	129	127	133	144	144	1.42.	145
	144	134	132	144	1 1 1	127	-12	141	124	137	1 40	120	134	141	140	120	1.54	143	140	141	14:1	143	121	1.1.1	-121-
55-	122	135	136	119	121	121	134	136	135	125	133	136	121	125	130	13.7	1 10	144	136	143	151	144	144	1-7	15)
56-	137	135	118	127	133	120	132	137	135	135	1 3 3	1 17	134	1 38	144	135	143	134	142	144	141	142	1:4	151	125
								1.18																2 2 A 10	

Figure 10. A portion of the vidicon image of the spectrum of ξ^2 Ceti from about 0.5 μ to over 0.6 μ . Note spatial spreading of image (vertically). The star is centered in row 32.

SX2CTIL

	1	- 7		4	5	6	. 7	8	9	10	11	12	13	
1-	315. 5.	4 3	4 7 10	\$24.7-4	519.92*	505.111	5.7.544	495.475	5 4.195	51 . 36	497.337	491.379	487.122	467.32
2-	65.476	11.571		128.448	35.361	9:.440	99.479	104.000	+6.912	95.749	93.933	+9.5FC	73.4.	\$1.50
3-	17.203	28.064	41.324	42.677	22.481	25.562	28.9 7	21.992	41.769	41.238	4 .251	33.163	17.599	11:47 -
4-	7.6 /	1.125	19.848	17.7:4	16.121	12.199	11.460	9.142	17.813	14.100	10.804	5.642	0.743	1.00
9-	2.745	9.861	10. 20.3	6.729	7.1.0	6.007	4.117	5, 682	11.411	F.876	6.4.26	3.215	0.000	5.02
6-	12.097	8	11.1 3	2.437	2.117	3.534	3.976	2.441	4.399	6.737	6.97.1	0.000	0.000	0.00
-1-	0.202	1.212	1.271	.0. /	. 1.463	3.595	4.555	1.320	11.514	1 .324	4.04i	0.206	0.000	0.00
	4.713.	4.364	3+454	3.6 18	2.576	2.363	1.295	4.269	0.372	C.961	1.690	0.198	0.000	5.00
9-	3.117	8.647	3.673	1.2.4	1.558	2.232	1.478	2.112	1.363	2.114	1.844	0.028	(. ?33	0.00
	6.197	2.323	0.125	1.45	2.627	1.040	.7 2	4.967		2.242	C.000	0.000	· • 0 · ·	0.20
11-	2.943	3.834	1.646	1.5.8	3.669	C.579	0.560	0.000	6.196	0.274	C.C.C	0.000	0.013	C.00
15-			1.1.14		0.712	0.6.34		1.100	4.399	1.978	C.240	Q • Q (Q	r.ecc	0.00
14-	9.447	1.583	0.257	1.2 (0.000	0.000	2.101	2.471	3.211	0.147	1.349	0.000	0.0.0	0.00
15	3.44	3. 907	C+113	0.407	4.204	0.351	3.427	2.332	1.440	0.155	0.000	0.0.0	0.000	1 44
16-	3.270	3.963		0.347	0.3/3	6.490	0.004	0.000	0.020	1 100	0.000		0.000	1 36
17-	1 203	1 201	0.000	0.2.3	1 34.3	. 670	1 240	6	1.3/3	0.636	4.106		0.030	
1	1 204	2.266	6.6.6	0.012	1.342	0.000	A 143	0.154	0.204	0.624	0.000	0.000	0.000	30.00
12-	5.103	2.6.15	0.007	0.010	0.024	1.374	0.514	0.000	0.046	1 420	2 175		0.00	0.03
2	0.762	1.80	C.000	728	1.089	1.756	1.246	0.734	0.000	0.024	0.0.0	0.0.0	0.000	0.77
21-	1.936	2.015	6.0.0	1. 1.4	0.663	1.165	0.735	6.194	1.015	0.177	0.511	0.000	0.010	
22-	4.512	1.171	C. 100	0.355	0.016	0.103	0.618	0.734	3.515	2.112	0.82%	0.000		0.
73-	1.226	1.764	6.000	1.115	2.309	2.507	1.809	1-432	1.952	2.903	0.000	0.000	0.000	0.00
24-	1.4 4	1. 71		7.4.11	0.579	0.165	0.009	0.418	1.033	0.236	C. 272	0.000	0.010	0.00
23-	5.144	3. 341	2.019	1. 340	6.229	0.136	1.005	0.184	0.320	0.000	0.000	0.000	0.000	0.00
14-	1.223	.611	0.011	3.045	0.083	6.675	0.000	1.199	0.413	9.024	2.000	3.000	0.000	0.12
21-	1. /07	3. 106	0.023	2.222	C. 725	6.324	6.569	1 74	1.776	2.584	2.202	0.000	0.0.0	0.00
-85	1.028	2.153	0.007	1.777	(.782	0.3(3	C.009	2.991	3.179	1.333	0.5.3	0.000	0.050	3.00
2.3-	0.112	0.550	0.000	5. 180	4.512	0.169	15.500	13.119	9.283	4.876	1.509	2.000	0.000	0.06
3 - ·	1.150	1.060	11.117	4.9.484	18.571	95.950	108.160	120.512	120.445	111.197	63.749	62.6.9	40.000	32.221
11-	4.913	13.983	114.153	11. 847	551.710	120.357	815.215	935.781	929.018	651.12:	154.748	607.217	555.1.1	47.251
52-	5.814	\$9.495	498 - 28	1201.647	1951.6 1	2353.964	263 .129	2925.239	2464.294	2641.002	2659.112	2491.456	27 792	1010. 3
·	5.99%	:3.615	e11.48*	2:23.7-2	\$ 15.479	3668.541	4056-195	4466.492	4552.:47	4464.301	4364.4 5	3614.543	3418.51:	3:45.478
34-	5.834	-1.007	41.4.1.51	1125.650	1011.617	2265.134	2576.136	2618.558	2254.633	2717.977	2400.230	23.00.044	1. 30.048	1851:
5.1-	4.874	22.957	2.1.1.27	404.6.3	631.461	787.384	9 2.716	1 10.430	1 9.7 5	1111.312	1115.98	1 84.440	1-13.769	974. 53
: 1-	2.429	12.817	110.301	271.25	266.051	357.481	341.267	442. 41	441.491	524.346	536.829	5. 7.613	50.041	-71 92
37-	1.708	5+137	41.44 >	#4.105	118.508	141.833	153.197	122.011	197.232	2-1.605	210.044	2.4.000	166.604	17 87-
5-1-	2.925	3.444	7.101	13.315	37.361	5 . 172	56.631	56.452	64.094	57.668	25.947	5.51	29.016	12.550
31-	1.256	1.9.3	0.+94	5.634	16.757	11.751	16.162	15.576	2.809	2.269	G.000	3.01C	6.6.5	0.000
	1.194	4.49.	1.006	0.397	1.107	0.912	0.007	1.041	C.960	0.201	0.000	0.0.0	0.000	0.017
•1-	1.6.77	1.003	1.037	0.257	0.426	0.214	0.147	0.312	0.000	0.614	0.000	0.000	0.011	0.043
	1 677	1.157	0.4 4	7.530	1.360		0.018	0.000	0.000	0.000	0.00	0.01.0	C.C00	0
	2 1 1 2	2 20	1.764	0.022	0.000	0.344	6.150	0.000	6.000	1.133	0.000	0.303	0. 10 1	0.106
	0.55	5.203		1.504	N. UC9	1 410	1 221	0.179	0.000	0.389	0.000	0.000	0.000	0.00
4-	1.66'	1.945	1.057	0.419	1 119	(174	0.376	0.214	0.000	0.000	1.340	0.024	0.013	0.000
T-	2.40 1	1.11.	0.558	0.002	1 366	0.640	C 707	2 451	0.000	0.034	1.347	0.028	2 212	1.1.0
	1.408	0.771	1 6 2 2	4 447	1.034	4.051	1 540	0 463	1 422	1 424	0.023		2.3/1	0.1.7
-1-	1.345	6.115	4.561		0.012	A. 455	0.000	0.000	1,273	0.000	1 922	0.00	0.3.14	6.092
SC-	3.575	1.174	1,172	6.610	0.967	0.641	1.074	1.652	0.000	0.024	1.1.21	0.500	3 401	12.41
-1-	1.644	0.515	1.9/.2	2.044	1.694	2. 199	0.551	2. 104	1. 141	0.000	0.000		0.001	1. 20
52-	2.512	1.334	7.262	4.305	0.223	1.474	0.000	1.000	0.620	0.310	1.0/3	1.514	7.633	7.13
53-	4.267	5. 775	1.677	1.698	0.006	0.755	0.000	0.707	1.073	1.605	3.134	13.072	12.646	7.13
-4-	3.827	1.205	6.235	1.517	4.496	1.688	0.716	2.671	1.477	1.144	3.000	4.7	1.0.5	
5-	2.538	2.162	1.399	9.018	1.187	.124	0.000	0. 167	0.000	1.581	6. 127	10.320	9.344	1.13
6	1.797	. 1.622	3.212	1.845	0.343	0.716	C.018	0.679	0.000	2.936	5.395	13.022	9.014	
1.11														5 5 5 5 S

Figure 11. A portion of the processed image of ξ^2 Ceti from 0.35 μ to 0.70 μ . Each image element represents intensity per ten angstroms averaged over a 250 angstrom resolution element. The background was first subtracted out of the vidicon image.

SX2CTLL

and a	1	. ,		4	5	6	. 7	8	9	10	11	12	13	. 14	•
1-	315. 5.	4 3	4 11 . 710	\$24.7-4	519.92*	505.111	5.2.544	495.475	5 4.195	51 . 36 .	497.337	491.379	487.122	467.32	-
2-	65.476	11.571	7 15	128.448	95.361	9:.441	99.479	104.008	46.912	95.749	73.933	. P9.5/C	73.4.	\$1.50.	
3-	17.2.3	28.064	41.324	42.677	22.481	25.562	28.9 7	21.492	41.769	41.238	4 .251	\$3.163	17.599	11.47.	
4-	7.6 /	1.125	14.848	17.7:4	16.121	12.199	11.460	9.142	17.813	14.100	10.804	5.642	0.743	1.00	
5-	2.745	9.861	10. 20.3	4.720	7.1.16	6.007	4.117	5, 682	11.411	F.876	6.4.16	3.215	0.000	5.02	
4-	12.001	8	11.1 3	2.437	2.117	3.534	3.976	2.441	4.399	6.737	6.974	0.000	0.000	0.00	
-1-	0.202	1.212	1.271	.0. /	1.463	3.595	4.555	1.320	11.514	1 .324	4.040	0.206	0.000	0.00	
-	4.713.	4.364	3*454	3.6 18	2.576	2.363	1.295	4.269	0.372	C.961	1.690	0.198	0.000	5.00	
9-	3.117	2.647	3.673	1.2.4	1.558	2.232	1.478	2.112	1.363	2.114	1.844	0.028	(. ?33	0.00	
	6.199	2.323	0.125	1.45	2.627	1.040		4.967		1.242	C.100	0.2.10	C.0	0.00	
11-	2.943	3.834	1.646	1.5.8	3.669	C.579	0.560	0.000	6.196	0.274	2.0.0	0.000	0.010	C.00	-
15-			1.4.44		0.712	0.634		1.100	4.314	1.978	C.24.	Q • Q • Q	r	0.00	-1
14-	9.441	1.043	0.257	1.2 1	0.000	0.000	2.101	2.471	3.211	0.147	1.349	0.000	0.0.0	0.00	1
1.5	3. 100	3. 907	C+113	0.907	4.204	0.351	3.427	2.332	1.440	4 340	0.000	0.0.0	0.000	1 40	1
16-	3.276	1.963		0.347	0.375	6.490	0.00	0.000	0.020	1 100	0.000		0.000	1 36	1
17-	1 203	1 201	0.000	0.2.3	1.343	. 670	1 240	6.000	0.174	0.636	4.106		0.030	0.00	4
1	1.204	2.266	5.6.6	0.012	0 004	0.000	A 143	0.156	0.207	0 437	0.000	0.000	0.000	30.00	-
13-	5.103	2.615	0.047	0.842	0.928	1. 376	0.514	9.000	0.046	1.430	2.175	0.000	0.01	0.03	٦
2	0.762	1.80	C.000		1.089	1.756	1.246	0.734	0.000	0.024	0.0.0	0.0.0	0.000	0.72	1
21-	1.936	2.015	6.0.0	1. 1.4	0.613	1.165	0.735	6.194	1.035	0.177	0.573	0.000	0.010		1
22-	4.512	1.171	C. 100	0.35	0.016	0.103	0.618	0.734	3.515	2.112	0.82%	0.000		0	1
73-	1.226	1.764	6.000	1.115	2.309	2.507	1.809	1-432	1.952	2.903	0.000	0.000	0.000	0.00	1
24-	1.4 9	1. 71		7.4.11	0.579	0.165	0.009	0.418	1.033	0.236	C. 275	0.000	0.010	0.00	1
23-	5.144	5. 341	2.019	1. 340	0.229	0.136	1.005	0.184	0.324	0.000	0.000	0.000	0.000	0.00	1
15-	1.223	.611	0.011	3.255	0.083	6.675	0.000	1.199	0.413	9.024	0.000	3.000	0.000	0.1.2	1
21-	1. /07	3. 106	0.023	2.222	C.725	6.324	6.569	1 74	1.776	2.524	2.202	0.000	0.0.0	0.00	1
-89	1.028	2.155	0.007	e.777	(.782	0.3(3	C.009	2.991	3.179	1.333	0.523	0.000	0.050	3.00	i
2 3-	0.112	0.550	0.000	5. 180	4.512	0.169	15.500	13.119	9.283	4.876	1.500	2.000	0.000	0.00	1
· - ·	1.750	1.060	11.119	49.485	18.571	95.950	108.160	120.512	120.445	111.197	63.749	62.6.9	40.000	32.221	1
11-	4.913	13.983	114.153	31 847	551.710	120.357	815.215	935.781	929.018	651.12:	154.248	607.217	555.1.1	47. 201	1
\$2-	5.814	\$9.495	498 - 28	1201.647	1951.8 1	2353.964	263 .129	2925.239	2464.294	2641.002	2659.112	2491.456	27 792	1010. 3	
3.7-	5.99%	:3.615	611.48-	2:25.7-2	\$ 15.479	3668.541	4056-195	4466.492	4552.:47	4464.301	4264.4 5	3004.543	3418.51:	3:49 78 .	
34-	5.83%	-1.007	41,4 . 1.51	1125.650	1011.617	2265.134	2576.136	2018.550	2254.633	2717.977	2400.230	23.00.033	1. 10.048	1854.41	1
5.1-	4.874	22.957	2.1.1.1.77	404.6.3	631.461	787.384	9 2.716	1 10.430	1 9.75	1111.312	1115.98	1 \$4.440	1 13.769	975. 53	1
	2.429	12.817	110.301	271.25	260.051	357.481	341.267	442. 41	441.991	524.346	536.829	5. 1.613	20.0041	-77. + 92	-
37-	1.708	5+137	41.44 >	#4.105	118.508	141.833	153.197	122.011	197.232	2-1.605	210.044	2.4.000	166.604	17 # 1-	1
5	2.925	3.444	7.101	19.315	37.361	5 . 172	56.631	56.452	64.094	57.668	25.947	5.51	29.016	11.550	1
31-	1.256	1 - 9 - 3	0.194	5.634	16.757	11.751	10-162	15.576	2.809	2.289	C.000	3.010	6.6.2	0.000	i
•0-	1.194	4.49.	1.006	0.391	1.107	1.912	0.007	1.041	C.960	0.201	0.000	0.0.0	0.000	0.017	1
	1.6.77	1.003	1.037	0.257	0.426	0.214	0.147	0.312	0.000	0.614	0.000	0.000	0.011	0.043	1
	1 627	1.137	0	1.530	1.360		0.116	0.000	C.000	0.000	0.0.0		C.C00		-
4-	2 1 1 2	2 24	1.364	0.044	0.000	0.344	6.150	0.000	0.000	1.131	0.000	A 000	0.000		
	0.55	3.25	1	1.004	N. UC. 9	1 410	1 221	0.114	6.000	0.369	0.000	0.000	0.000		
4-	1.66'	1.945	1.057	0.419	1 119	(174	0.376	0.214	0.000	0.000	0.000	0.024	0.013	0.000	
T-	2.40 1	1.11.	0.559	0.002	1 308	0.640	C 757	2 451	0.000	0.000	0 8.1	0.028	3 317	1.1.0	
	1.408	0.771	1 6 2 2	4 447	1 034	4.051	1 560	0 163	1 422	1 424	0.020	1. 12	2.3/1	0.1.7	
-1-	1.345	6.115	4.561		0.012	A. 455	0.000	0.000	1.273	0.000	1 927	0.00	0.3.14	6.092	
- J	3.575	3. 174	1,172	6.610	0.967	0.641	1.074	1.652	0.000	0.024	1.1.1	0.500	3 401	12.41	F
1-	1.644	0.515	1.9/.2	2.044	1.694	2. 199	0.551	2. 104	1. 141	0.000	0.000		0.001	1. 55	1
2-	2.512	1.334	7.21.2	4.305	0.223	1.474	0.000	0.000	0.620	0.310	1.0/3	1.514	7.633	7.13	1
- 1	4.267	5. 775	3.657	1.648	0.006	0.755	0.000	0.707	1.033	1.605	3.124	13.072	12.646	7.13	1
4-	3.827	1.205	6.235	1.517	4.496	1.688	0.716	2.671	1.477	1.144	3.000	4.7	1.0.5		1
5-	2.538	2.162	1.379	9.018	1.187	0.124	0.000	0. 167	0.000	1.581	6. 127	10.320	9.344	1.13	1
-04	1.797	1.622	3.212	1.845	0.343	0.716	C.018	0.679	0.000	2.936	5.395	13.022	9.014		1
1000															

Figure 11. A portion of the processed image of ξ^2 Ceti from 0.35 μ to 0.70 μ . Each image element represents intensity per ten angstroms averaged over a 250 angstrom resolution element. The background was first subtracted out of the vidicon image.

above the background. After this integration, the spectrum vector is punched out onto cards for plotting and further processing. A more advanced version of this processor will incorporate the plotting, ratioing, and other functions into one DIPSYS subsystem. where only disk files will be used.

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The final procedure needed for good spectral reflectivity data of the surface of a planet is to know from what part of the surface the spectrum originates. A photograph is taken through the eyepiece, looking at the slit in a mirror tilted 45 degrees to the optical axis of the telescope (the first surface in Figure 3). A similar logging arrangement is used for photometer data. A plotting program has been written to create Calcomp plots of the coordinate grid of Mars (or any other planet) projected onto a disk using the physical ephemeris of the planet from The American Ephemeris and Nautical Almanac and the time of observation in Universal Time. Figure 12 is a block diagram of the program, while Figure 13 is a typical, although smaller than normal. output. To position the spectrometer slit on the disk of the planet, the negative of the photograph of the telescope image is projected onto the grid, and the slit marked by hand. At this point the original vidicon images have been reduced to constant resolution spectra of stars and known positions on Mars; and reduction to spectral reflectivity data, as well as testing, can begin.





IV. Analysis of Data

The first major attempt to use the vidicon spectrometer to take spectra for reflectivity work occurred during the opposition of Mars during October, 1973. On two consecutive nights the Mauna Kea eighty-inch reflector was trained on the planet Mars, and about 75 spectra were taken, as well as an equal number of spectra of the standard stars Alpha Lyra and Xi 2 Ceti. Xi 2 Ceti was chosen because it was near Mars in the sky, while Alpha Lyra has a spectrum which is well known and is used to calculate planet/sun ratios to get reflectivity. Figure 14 demonstrates the reduction methods used to get spectral reflectivities from raw intensity To avoid airmass reductions, spectra of Alpha Lyra and spectra. Xi 2 Ceti were taken when the two stars were at the same airmass, Since star/star ratios exhibit little variation with low 1.38. airmass changes, the ratio of the two stars obtained from these spectra can also be used to reduce reflectivities at other airmasses. Before any data was reduced to reflectivities, extensive testing was done to see whether the data would be usable. This portion of the thesis will describe that work, using the best results obtained to date.

Figure 15 shows a high resolution spectrum of Alpha Lyra which has been averaged over 250 angstrom segments to simulate the spectrometer output. Figure 16 is an Alpha Lyra spectrum from the vidicon spectrometer from which the vidicon response has been



Figure 14. Production of spectral reflectivity from raw spectra. Air mass correction not not needed if objects to be ratioed are at the same air mass.







SALTR87 / VIDLEON

Figure 16. a Lyra spectrum from vidicon spectrometer with vidicon response (Figure 2) divided out.

removed. Note that the peak is shifted to a slightly longer wavelength and that the shape is generally broader to about 0.7 To test the repeatability of the data, pairs of spectra microns. of the same star were ratioed to each other. Results of one such pair are shown in Figure 17 (all ratios plotted are normalized to 1.0 at 0.575 microns). Figure 17a is the ratio of two Alpha Lyra spectra with similar airmasses (1.40/1.38), but different exposure times (5sec/1sec). If the response of the system were perfectly linear, that is, if intensity recorded from a given source is a linear function of the integration (exposure) time, the curve would be flat. It is obvious that it is not; however, the relatively flat region corresponds with the peak intensities of the spectra, so it may be that low level signals are nonlinear representations of the intensity received from the star. To test this idea, a 'pedestal' was set up under the spectrum. AII intensities below a certain value would be ignored, and possibly. the nonlinear features of the curve would go away. Figures 17b and 17c show the results of installing pedestals of 300 and 400. respectively (the maximum intensity registerable is 4095). а pedestal of 300 seems to help from 0.5 to 0.8 microns, but a larger pedestal doesn't help at all. Figure 18 shous a similar ratio for two Xi 2 Ceti spectra with slightly different airmasses (1.67/1.32) and different exposure times (20sec/15sec). Once again the curve is relatively flat over the peak in incoming energy, this time from almost 0.4 to 0.8 microns. (Figure 19 is a



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Figure 17a. Ratio of two α Lyra spectra, all elements above background included.







Figure 18. Ratio of two ξ^2 Ceti spectra, including all image elements above background.

typical Xi 2 Ceti spectrum). this time, however, there is a smooth upturn which has some undetermined significance. Thus, star ratios seem to be usable, at best, from 0.4 to 0.8 microns.

Now that there is some idea as to the reliability range of the spectrometer, indefinite though it may be, the Mars spectra can be observed. Figure 20 is a typical Mars spectrum, summed over five vidicon elements down the slit. Note that the peak is in the red, rather than the blue like the two stars' spectra. This is because the stars are both of spectral type A0, while the sun, which is providing the light which is reflected from Mars is a cooler, redder type G. Figure 21 shows a saturated spectrum of Mars. The peak intensity of 4095 is surpassed from 0.5 to 1.0 microns, although around 1.1 microns, the signal is unsaturated. Originally it was thought that the unsaturated portions of a saturated spectrum could be used to extend the range of an unsaturated spectrum which had a very low signal beyond 1.1 microns. The data show, unluckily, that there is little or no overlap between the good signal from one and the good signal from the other type of spectrum. Once again, an attempt was made to do away with low, nonlinear signals with a pedestal. Figures 22a, b, and c show the progressive changes as pedestals of 300 and 400 are subtracted from the original spectrum. Ratios of Mars images seem to be more consistent than those of star images. Figures 23a, b, and c and 24a, b, and c are the results of ratioing different images of Mars to each other. The three images used



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Figure 19. A typical ξ^2 Ceti spectrum. Note that the peak is at a longer wavelength and the shape is broader than α Lyra.





Figure 21. An overexposed spectrum of Mars. Arrows indicate intensities reading greater than 4095 in at least one element of the image which went into the resolution element.



Figure 22a. Mars spectrum









were taken within 15 minutes of each other. The same portion of the image was used in each case. Each is a one minute exposure. Note the flat curve from 0.5 to 1.1 micron, indicating better repeatability than for the stars, possibly due to more signal above a nonlinear level. As the pedestal is increased, some of the apparently good data is lost, but the noise is gone by the time a pedestal of 400 is used (c). The Mars spectra are probably recoverable.







Figure 23b. Ratio of two Mars spectra, each of which has a pedestal of 300.







Figure 24b. Ratio of two Mars spectra, each of which has a pedestal of 300.



V. Recommendations for Future Use of the Vidicon Spectrometer

Although it appears that it will be impossible to do spectral reflectivity work using the vidicon spectrometer due to an inability to meaningfully ratio stars and planets over a useful range, the instrument has advantages which will make it worthwhile to develop it. The combination of good spectral resolution (250 angstroms or better, compared to 300 angstroms for a filter photometer), with complete spectral coverage and high spatial resolution indicate much promise. It appears that the limiting factor will be the response function of the vidicon tube, with its nonlinearities in wavelength and intensity. Once more lab work is done to quantify knowledge about this problem, the instrument will be ready to gather more data. Another problem which may affect the star spectra is the problem of differential diffraction of the Different wavelengths, star's light by the earth's atmosphere. diffracted at slightly different angles would show up at different positions in the smeared out star spectrum, and if the slit is smaller than the apparent diameter of the star, part of the star's spectrum would be lost, in a wavelength-preferential manner. The solution is to widen the slit; although the spectral resolution at the vidicon would be reduced, the spectrum would be much more reliable. But what about the Mars data from Mauna Kea? With the high spatial resolution and apparent good response of the vidicon, something should be recoverable. The planet in the slit occupies

up to 35 elements in a vidicon column when it is about 23 arc seconds in diameter, and the slit is two elements wide, so, with good seeing of 1.5 seconds or less, there are fifteen spectra per spectrometer image. Luckily, the slit passes over some photometer spots that were taken within days of the vidicon spectrometer run, allowing relative reflectivities to be obtained, basically extending the photometer data for more complete surface coverage. For example, Figure 25 shows the position of the slit on the planet's disk during one run. This one slit passes through the Coprates canyon as well as a large dust storm to the southwest of Coprates. Using a photometer spot as a standard and modifying resolution to match the photometer, some interesting data should be forthcoming.



Figure 25. Position of one set of spectra across the disk of Mars. Latitude and longitude of the sub-earth point, S, given.

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Determination of Martian Surface Spectral Reflectivity from 0.4 to 1.1 μ Using a Vidicon Spectrometer

A Proposal for a thesis toward the degree of Master of Science

By Douglas J. Mink

I propose to analyze the spectral reflectivity of Mars from 0.4 to 1.1μ using the vidicon spectrometer system developed at the MIT Planetary Astronomy Laboratory. This system consists basically of a slit at the focus of a telescope, from which light goes through a low resolution prism. The spectrum produced is imaged on a vidicon image tube which is read out onto magnetic tape. The image produced has wavelength nonlinearly along one axis and spatial variation along the slit as the other axis. A prism dispersion function is used to calibrate wavelength to image column coordinate, and a photograph of the slit superimposed on the telescope image of the planet is used to determine spatial position.

About one hundred spectra were taken at Mauna Kea Observatory during the opposition of Mars in October of 1973 by members of the Planetary Astronomy Laboratory staff. Reduction of the data involves ratioing the intensity of light received from the planet, through known standard stars, to the sun[®]s emitted radiation, thus obtaining the reflectivity of the planet[®]s surface as a function of wavelength. This function has been shown to be an indication of the composition of the surface. Analysis has included hand-reduction of spectra and development of a computer program to plot a coordinate grid for a planetary disk from physical ephemeris data. A computer reduction system is being developed to handle the data.

Geological implications of the reflectivity spectra will be discussed, based on comparison with spectral reflectivity analysis of various minerals. Mineral content of Martian surface materials will be discussed in relation to various theories of Mars' composition, although extensive interpretation is beyond the scope of this thesis.